

## Real-time experimental control of a system in its chaotic and nonchaotic regimes

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Current model-independent control techniques are limited, from a practical standpoint, by their dependence on a precontrol learning stage. Here we use a real-time, adaptive, model-independent (RTAMI) feedback control technique to control an experimental system — a driven magnetoelastic ribbon — in its nonchaotic and chaotic regimes. We show that the RTAMI technique is capable of tracking and stabilizing higher-order unstable periodic orbits. These results demonstrate that the RTAMI technique is practical for on-the-fly (i.e., no learning stage) control of real-world dynamical systems. [S1063-651X(97)50710-0]

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Model-independent chaos control techniques, the first of which was developed by Ott, Grebogi, and Yorke [1], have been applied to a wide range of physical and physiological systems [2–11]. Recently, similar techniques have been developed to stabilize underlying unstable periodic orbits (UPO's) in nonchaotic dynamical systems [12–18]. In general, model-independent control techniques use feedback perturbations to stabilize a dynamical system about one of its UPO's. In contrast to traditional control techniques (which require knowledge of a system's governing equations), model-independent techniques are inherently well-suited for "black-box" systems because they extract all necessary control information from a premeasured time series. The flexibility of model independence in current dynamical control techniques, however, does not come without limitations. The precontrol time-series measurement and the corresponding system-dynamics estimation comprise a "learning" stage. For some real-world systems (e.g., cardiac arrhythmias), however, unwanted dynamics must be eliminated quickly, and thus the time required for a learning stage may be unavailable.

Recently, a real-time, adaptive, model-independent (RTAMI) control technique, was developed [19] to stabilize flip-saddle UPO's in chaotic and nonchaotic dynamical systems that can be described effectively by a unimodal one-dimensional map. Because the RTAMI technique does not require a precontrol learning stage (i.e., it operates in real time) it is practical for on-the-fly control of dynamical systems. In Ref. [19], the RTAMI technique was successfully applied to a wide range of model systems in their nonchaotic and chaotic regimes. Here, we apply the RTAMI control technique to an experimental system — a driven magnetoelastic ribbon — in its nonchaotic and chaotic regimes.

The RTAMI technique is designed to stabilize the flip-saddle unstable periodic fixed point  $\xi^* = [x^*, x^*]^T$  (where superscript  $T$  denotes transpose and  $[x^*, x^*]^T$  is a  $2 \times 1$  column vector) of a system that can be described effectively by a unimodal one-dimensional map  $x_{n+1} = f(x_n, p_n)$ , where  $x_n$  is the current value (scalar) of one measurable system variable,  $x_{n+1}$  is the next value of the same variable, and  $p_n$  is the value (scalar) of an accessible system parameter  $p$  at index  $n$ . The control technique perturbs  $p$  such that  $p_n = \bar{p}$

+  $\delta p_n$ , where  $\bar{p}$  is the nominal parameter value, and  $\delta p_n$  is a perturbation [3,4,20–22] given by

$$\delta p_n = \frac{x_n - x_n^*}{g_n}, \quad (1)$$

where  $x_n^*$  is the current estimate of  $x^*$ , and  $g_n$  is the control sensitivity  $g$  at index  $n$ . The ideal value of  $g$  is the sensitivity of  $x^*$  to perturbations:  $g_{\text{ideal}} = \delta x^* / \delta p$ . As described in Ref. [23], control can be achieved for nonideal values of  $g$  in the range  $|g|_{\text{min}} \leq |g| \leq |g|_{\text{max}}$ . (Prior to control, it is not possible to determine  $g_{\text{min}}$  or  $g_{\text{max}}$  without an analytical system model or a learning stage.)

As shown in Fig. 1, the current state point  $\xi_n$  would move,

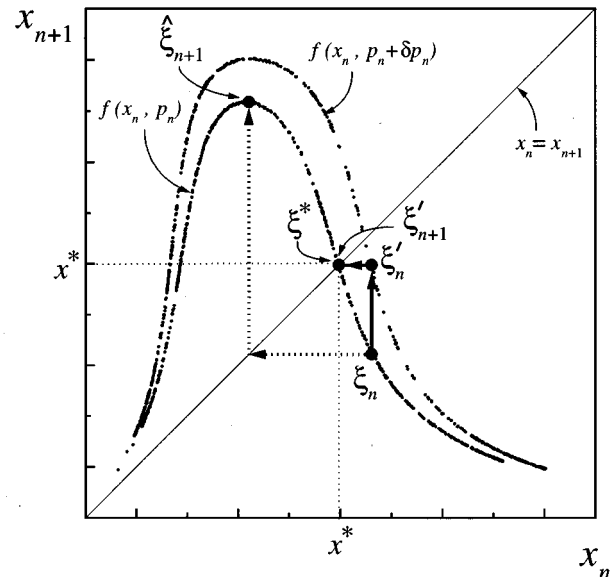


FIG. 1. First-return map showing that  $\delta p_n$  [Eq. (1), with  $g = g_{\text{ideal}}$ ] shifts the map from  $f(x_n, p_n)$  to  $f(x_n, p_n + \delta p_n)$  such that the next system state point is forced to  $\xi'_{n+1} \approx \xi^*$ , rather than to its expected position  $\hat{\xi}_{n+1}$ . These data, shown for illustrative purposes, are from simulations of the Belousov-Zhabotinsky chemical reaction.

in the absence of a perturbation (i.e.,  $\delta p_n = 0$ ), to  $\hat{\xi}_{n+1}$  (via the dotted arrow). However, the control perturbation of Eq. (1) (corresponding to  $g = g_{\text{ideal}}$ ) shifts  $f(x_n, p_n)$  to  $f(x_n, p_n + \delta p_n)$  such that  $x_n$  maps to  $x'_{n+1} = x^*$ , instead of  $\hat{x}_{n+1}$ . On the first-return map, this shift appears as the movement of  $\xi_n$  to  $\xi'_n$  (via the solid vertical arrow in Fig. 1). When the map is returned to  $f(x_n, p_n)$  for the next iteration, the next state point will be  $\xi'_{n+1} \approx \xi^*$ , as desired for control. In a physical system, due to noise, measurement errors, and the instability of  $\xi^*$ , perturbations are required at each iteration to hold  $\xi_n$  within the neighborhood of  $\xi^*$ .

Learning-stage dependent techniques use static values for  $x^*$  and/or  $g$ , as estimated from a precontrol time-series measurement. In contrast, the RTAMI technique repeatedly estimates  $x^*$  and  $g$ . In addition to eliminating the need for a learning stage, this adaptability allows for the control of non-stationary systems. When control is initiated,  $g$  can be set to an arbitrary value (with the restriction that the sign of  $g$  must match that of  $g_{\text{ideal}}$ ; if the signs do not match, control will fail). After each measurement of  $x_n$ ,  $x^*$  is estimated using

$$x_n^* = \sum_{i=0}^{N-1} \frac{x_{n-i}}{N}, \quad (2)$$

where  $N$  is the number of past data points included in the average [24]. Equation (2) converges to  $x^*$  because consecutive  $x_n$  alternate on either side of  $x^*$  due to the flip-saddle nature of  $\xi^*$ .

At each iteration, after  $x^*$  is re-estimated via Eq. (2), the RTAMI technique evaluates whether the estimate of  $g$  should be adapted. The value of  $g$  is not adapted if the desired control precision  $\epsilon$  has been achieved. Control precision has *not* been achieved if

$$|x_n - x_{n-1}^*| > \epsilon \quad (3)$$

is satisfied by at least  $L$  data points out of the  $N$  previous data points, where  $x_{n-1}^*$  is the estimate of  $x^*$  that was targeted for a given  $x_n$ . The  $L/N$  factor is used [instead of a single evaluation of Eq. (3)] to reduce the influence of noise and spurious data points.

If the desired control precision has not been achieved [i.e., Eq. (3) has been satisfied by at least  $L$  data points out of the  $N$  previous data points], then the magnitude of  $g$  is adapted in accordance with the expected perturbation dynamics [19]. If  $g = g_{\text{ideal}}$ , then the perturbation moves the state point from its current position  $\xi_n$  to  $\xi^*$  (as in Fig. 1). If  $|g|$  is too large (i.e.,  $\delta p$  is too small), then the state point moves from its current position  $\xi_n$  to a position closer to  $\xi^*$  than would be expected without a perturbation. If  $|g|$  is too small (i.e.,  $\delta p$  is too large), then the state point moves from its current position  $\xi_n$  to a position on the same side of the line of identity. (This is in contrast to the expected alternation, due to the flip-saddle nature of  $\xi^*$ , of consecutive state points on either side of the line of identity.) The criterion

$$\text{sgn}(x_n - x_{n-1}) = \text{sgn}(x_{n-1} - x_{n-2}) \quad (4)$$

is satisfied when two consecutive state points ( $[x_{n-1}, x_{n-2}]$  and  $[x_n, x_{n-1}]$ ) lie on the same side of the line of identity. The RTAMI technique increases the magnitude of  $g$  (i.e.,

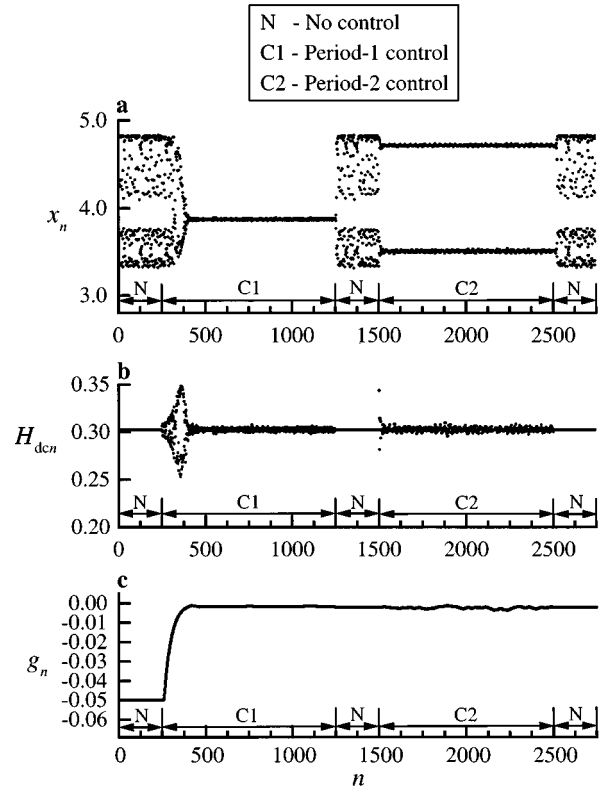


FIG. 2. (a)  $x_n$ , (b)  $H_{\text{dcn}}$ , and (c)  $g_n$  versus drive cycle  $n$  for a RTAMI control trial of the chaotic magnetoelastic ribbon. The respective control stages are annotated in (a), (b), and (c).

$g_{n+1} = g_n \rho$ , where  $\rho$  is the adjustment factor) if Eq. (4) is satisfied for at least  $L$  data points out of the  $N$  previous data points. As with the evaluation of control precision [Eq. (3)], the  $L/N$  factor is used [instead of a single evaluation of Eq. (4)] to reduce the influence of noise and spurious data points.

If the magnitude of  $g$  is not increased [as dictated by Eq. (4)], then the magnitude of  $g$  is decreased if  $\xi_n$  is not converging rapidly (at a rate governed by  $r$ ) to  $\xi^*$ . Specifically, the magnitude of  $g$  is decreased (i.e.,  $g_{n+1} = g_n / \rho$ ) if

$$\frac{1}{N} \sum_{i=0}^{N-1} \frac{|x_{n-i-1} - x_{n-i-2}^*| - |x_{n-i} - x_{n-i-1}^*|}{|x_{n-i-1} - x_{n-i-2}^*|} < r\% . \quad (5)$$

Equation (5) is satisfied if, on average, the distance  $|x_{n-i} - x_{n-i-1}^*|$  between a given data point  $x_{n-i}$  and its corresponding fixed-point estimate  $x_{n-i-1}^*$  is not at least  $r\%$  smaller than the distance  $|x_{n-i-1} - x_{n-i-2}^*|$  between the previous data point  $x_{n-i-1}$  and the previous fixed-point estimate  $x_{n-i-2}^*$ .

If neither Eq. (4) nor Eq. (5) is satisfied, then  $g$  is not adapted because  $x$  is properly approaching the estimate of  $x^*$ .

The experimental system we considered [25] consists of a gravitationally buckled magnetoelastic ribbon driven parametrically by a sinusoidally varying magnetic field. The ribbon is clamped at its lower end and its position  $x$  is measured once per drive period at a point a short distance above the clamp. The ribbon's Young's modulus can be varied by applying an external magnetic field. The applied magnetic field

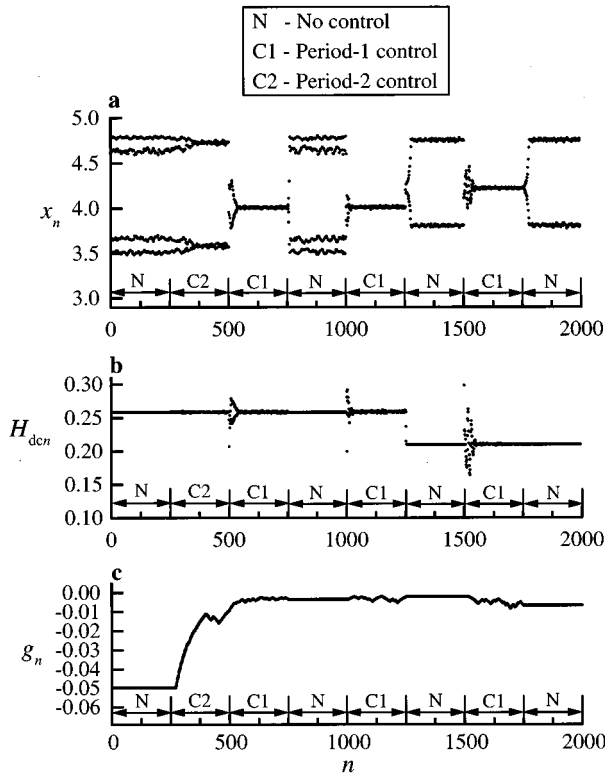


FIG. 3. (a)  $x_n$ , (b)  $H_{dcn}$ , and (c)  $g_n$  versus drive cycle  $n$  for a RTAMI control trial of the magnetoelastic ribbon in two different nonchaotic regimes [stable period-4 regime ( $1 \leq n \leq 1250$ ) and stable period-2 regime ( $1250 < n \leq 2000$ )].

is  $H_{app} = H_{dc} + H_{ac} \sin(2\pi ft)$ , where  $H_{dc}$  is the dc-field amplitude,  $H_{ac}$  is the ac-field amplitude, and  $f$  is the ac-field frequency. To apply the RTAMI control technique to the magnetoelastic ribbon,  $H_{dc}$  was used as the control parameter [i.e.,  $p_n \equiv H_{dcn}$  such that  $H_{dcn} = \overline{H_{dc}} + \delta H_{dcn}$ ].

Figure 2 shows a typical RTAMI control trial (with  $\overline{H_{dc}} = 0.302$  Oe,  $H_{ac} = 1.037$  Oe,  $f = 0.9$  Hz,  $N = 10$ ,  $\epsilon = 0.01$ ,  $L = 3$ ,  $r = 5\%$ , and  $\rho = 1.025$ ). At  $n = 250$ , following a period of chaotic ribbon motion (corresponding to a two-piece attractor), control of the unstable period-1 fixed point was activated. The initial control perturbations [Fig. 2(b)] were too small (because  $|g|$  was too large) to move the state point into the neighborhood of the fixed point (and hold it within that neighborhood) [Fig. 2(a)]. Thus,  $|g|$  was decreased [as dictated by Eq. (5)] until the magnitude of the perturbations increased and the state point converged to the unstable period-1 fixed point. Note that although Eq. (1) is only valid in the linear region of  $\xi^*$ , the value of  $g$  required to pull  $\xi_n$  into the neighborhood of  $\xi^*$  was also suitable for the stabilization of  $\xi^*$  (i.e.,  $|g|_{min} \leq |g| \leq |g|_{max}$ ). Also note that it is possible that the large parameter perturbations required to move  $\xi_n$  into the neighborhood of  $\xi^*$  could alter  $p$  to a regime where  $\xi^*$  is stable. However, because of the flip-saddle nature of  $\xi^*$ , consecutive perturbations (excluding those influenced by noise or when  $|g|$  is too small) are opposite in polarity, thereby ensuring that a parameter-regime change into the stable regime of  $\xi^*$  is followed by a parameter-regime change away from the stable regime of  $\xi^*$ . Thus, the large perturbations should not be mistaken for a

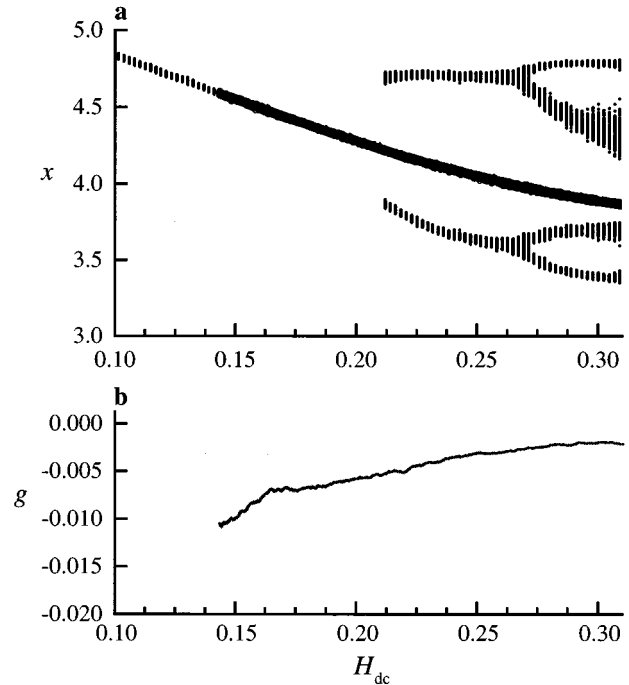


FIG. 4. (a)  $x$  versus  $H_{dc}$  for a RTAMI tracking trial (dark points) overlaid onto the corresponding bifurcation diagram. (b)  $g$  for the tracking trial shown in (a).

parameter-regime shift that is used to capture  $\xi^*$  when it is stable, in order to drag it back into the unstable regime.

Stabilization was maintained until  $n = 1250$ , when control was deactivated. At  $n = 1500$ , stabilization of the system's unstable period-2 fixed point was activated [26]. Period-2 stabilization was quickly achieved by updating the estimates for  $x_n^*$  and  $g$  and applying control interventions at every other iterate rather than at every iterate.

Figure 3 shows a RTAMI control trial (with  $\overline{H_{dc}} = 0.258$  Oe,  $H_{ac} = 1.037$  Oe,  $f = 0.9$  Hz,  $N = 10$ ,  $\epsilon = 0.01$ ,  $L = 3$ ,  $r = 5\%$ , and  $\rho = 1.025$ ) that demonstrates: (i) on-the-fly control of a system that is switched rapidly between different parameter regimes and (ii) stabilization of UPO's which underlie stable higher-period orbits in a nonchaotic system. At  $n = 250$ , following a period of stable period-4 ribbon oscillation, control of the system's underlying unstable period-2 fixed point was activated. After  $|g|$  was decreased, as dictated by Eq. (5), period-2 stabilization was achieved and maintained until  $n = 500$ , when the control target was switched from the underlying unstable period-2 fixed point to the underlying unstable period-1 fixed point. Period-1 stabilization was maintained until  $n = 1250$ , when control was deactivated and  $\overline{H_{dc}}$  was changed to  $\overline{H_{dc}} = 0.210$  Oe, corresponding to a stable period-2 oscillation. At  $n = 1500$ , period-1 stabilization was activated directly from the stable period-2 oscillation. Note that the magnitude of  $g$  increased and decreased [Fig. 3(c)], as dictated by Eqs. (4) and (5), for the different unstable periodic fixed points and parameter regimes.

In addition to controlling a dynamical system in its non-

chaotic or chaotic regimes, the RTAMI technique is capable of “tracking” [12–16,22] an unstable periodic fixed point from its stable period-1 regime through multiple period-doubling bifurcations into the chaotic regime, and vice versa (i.e., from its chaotic regime back to its stable period-1 regime). Figure 4 shows a tracking trial in which the RTAMI technique was used (with  $H_{ac}=1.037$  Oe,  $f=0.9$  Hz,  $N=10$ ,  $\epsilon=0.00$ ,  $L=3$ ,  $r=5\%$ , and  $\rho=1.001$ ) to track the unstable period-1 fixed point from  $\overline{H}_{dc}=0.311$  Oe (chaotic regime) to  $\overline{H}_{dc}=0.144$  Oe (stable period-1 regime). Figure 4(a) shows the tracking trial (dark points) overlaid onto the corresponding bifurcation diagram, while Fig. 4(b) shows the corresponding  $g$ . Note that  $|g|$  was largest (i.e., most negative) when the slope  $\delta x/\delta H_{dc}$  of the period-1 fixed point in Fig. 4(a) was largest, and  $|g|$  was smallest (i.e., least negative) when the slope  $\delta x/\delta H_{dc}$  of the period-1 fixed point was smallest. This further demonstrates (because  $g_{ideal} = \delta x/\delta H_{dc}$ ) that the RTAMI technique effectively adapts  $g$ .

The RTAMI control technique was unable to stabilize the unstable period-1 fixed point of the driven magnetoelastic ribbon in the chaotic parameter regime  $\overline{H}_{dc}>0.311$  Oe. This control failure resulted from the fact that the value of  $g$  required initially to move  $\xi_n$  into the neighborhood of  $\xi^*$  was not within the range of  $g$  values suitable for stabilizing  $\xi^*$ . This is in contrast to the case where  $\overline{H}_{dc}<0.311$  Oe (as de-

scribed for Fig. 2) in which the value of  $g$  required to pull  $\xi_n$  into the neighborhood of  $\xi^*$  was suitable for control (i.e.,  $|g|_{min} \leq |g| \leq |g|_{max}$ ). When  $\overline{H}_{dc}>0.311$  Oe,  $|g|<|g|_{min}$  was required to pull  $\xi_n$  into the neighborhood of  $\xi^*$ . Thus, once  $\xi_n$  entered the neighborhood of  $\xi^*$ , oversized perturbations [28] were delivered that promptly repelled  $\xi_n$  from  $\xi^*$  before the magnitude of  $g$  could be increased.

In this paper, we have shown that the RTAMI technique can be used to control an experimental system. Specifically, we have controlled the motion of a driven magnetoelastic ribbon in its period-2 regime, period-4 regime, and chaotic regime. We have demonstrated that the RTAMI control technique is capable of (i) on-the-fly control as a system is switched between parameter regimes, (ii) stabilizing higher-order UPO's, and (iii) tracking a UPO through multiple bifurcations. These results demonstrate that the RTAMI technique is versatile and practical for real-time control of real-world systems.

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- [27] Setting  $\epsilon=0.00$  is equivalent to eliminating Eq. (3) from the RTAMI algorithm. This simplifies the real-world applicability of the technique by eliminating a parameter (i.e.,  $\epsilon$ ).
- [28] The perturbations were oversized because  $|g|$  was too small for the neighborhood of the fixed point. This resulted in consecutive state points that were forced onto the same side of the line of identity.